Effects of pre-treatments on drying kinetics of sweet potato slices

Rufus Rotimi Dinrifo^{**}

(Agricultural Engineering Department, School of Engineering, Lagos State Polytechnic, Ikorodu. 23401. Lagos Nigeria)

Abstract: In this study, thin layer drying kinetics of sweet potato slices was investigated by using a hot air convective dryer operated at 50, 60, 70 and 80°C. Different treatments were given to samples of sweet potato slices: some were blanched in hot water at 100°C (WAT), others were dipped in sodium meta-bisulphite (SMB), while the rest were left untreated (UNT). The experimental drying data were fitted to four well known drying models: the Modified Page 1, Wang and Singh, Two Term Exponential and Approximation of Diffusion. Among the four models considered, the Modified Page 1 was found to best describe the drying kinetics of sweet potato slices. The effective moisture diffusivity of the samples was in the range from 7.76×10^{-9} m²/s to 1.2×10^{-8} m²/s. The values for activation energy, the energy necessary for the onset of the drying process, were 9.13 kJ/mol, 11.25 kJ/mol and 17.5 kJ/mol for WAT, SMB and UNT, respectively, indicating that it was easier to induce the water release process in the WAT and the SMB compared to the UNT samples.

Keywords: sweet potato, pre-treatment, drying kinetics, drying models

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1 Introduction

Sweet potato (Ipomea batatas) is a low-input tropical crop that has great nutritive and agronomic characteristics (Woolfe, 1992). Currently, Nigeria is the largest producer in Africa and the second largest producer of sweet potato tubers in the world, after China (FAO, 2008). Sweet potato is rich in complex carbohydrates, dietary fibre, iron, calcium and vitamins. The tubers are most frequently boiled, fried or baked. They can also be processed to make starch for ethanol production and as partial flour substitute for cake or bread producing. Many food products such as tomato sauce, ketchup, dried-cake, spongy cake, and biscuit utilize sweet potato as part of their ingredients (Zuraida, 2003). New uses such as for the production of noodles, cookies, doughnuts could increase the demand for sweet potatoes (Indrasari et

al., 1994).

Sweet potato tubers once harvested deteriorate rapidly, mainly due to physiological changes and mechanical damage during harvesting, transportation and handling. Besides, the tubers exhibit no dormancy and are susceptible to insect infestation. The very short storage life after harvest has been recognised as a limitation to the cultivation of the crop (Okaka, 1997). As a result, growers prefer to convert the tubers into more stable forms such as chips and flours so as to prolong the shelf life (Oyewole, 2002; Ayinde and Dinrifo, 2001). This is usually done by cutting the tubers into slices and drying them in the open sun or in an air-dryer.

Prior to drying, most food products are usually subjected to a some form of pre-treatments, among which are hot water blanching and sulphiting. Blanching helps to inactivate enzymes that may lead to quality degradation (Moreno-Perez, Gasson-Lara and Ortega-Rivas, 1996) and to improve the acceptability of the final product (Babajide et al., 2006). According to Senadeera et al., (2000) blanching also leads to structural softening and hence facilitates moisture removal. Hot

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^{*} Corresponding author: Rufus Rotimi Dinrifo, Agricultural Engineering Department, School of Engineering, Lagos State Polytechnic, Ikorodu. 23401. Lagos Nigeria; Email: rdinrifo@yahoo.com

water blanching and the use of chemicals such as sulphur, methyl and ethyl ester emulsions or alkaline pre-treatment in aqueous solutions of sodium hydroxide, sodium chloride, potassium and sodium carbonate, calcium chloride have been applied to overcome the waxy or fibrous barrier on roots, fruits and vegetables (Krokida and Moroulis, 2001; Doymaz, 2007; Doymaz and Pala, 2002).

Knowledge of the drying kinetics of biological materials is essential to the design, optimization and control of drying processes. Many authors have reported the drying characteristics of various agricultural or food products. Among these are the reports on tomato (Sacilik, Keskin and Elicin, 2006), yam (Sobukola, Dairo and Odunewu, 2008), carrot (Doymaz, 2004), okra (Sobukola, 2009). Iciek and Krysiak (1995) studied the effect of various parameters of convective drying on the quality of Irish potatoes. In addition, several thin layer models have been proposed for explaining the drying behaviour of these agricultural products. These equations allow the prediction of the process parameter as a function of time at any point in the drying process based on the initial condition. These include models for: potato slices, vam (Akanbi, Gureje and Adevemi, 1996), rice (Basunia and Abe, 1998), maize (Courtois et al., 1991; Falabella, Suarez and Viollaz, 1991), onions (Elustondo, Pelegrina and Urbicain, 1996; Faborode, Favier and Ajayi, 1995), plantain (Johnson, Brennan and Addo-Yobo, 1998), and apple (Chiang and Petersen, 1987). Diamante and Munro (1993) presented a model for the thin layer drying of sweet potato slices under solar

conditions. Since the industrial production of food products normally depend on artificial dryers, there is a need to investigate the drying kinetics of sweet potatoes under artificial dryer conditions. Also, since pre-treatments are important in industrial drying, their effects need to be investigated. Singh et al., (2006) investigated the effect of air temperature and pretreatments on drying kinetics of sweet potato slices. The authors considered pre-treatments using potassium permanganate solution and citric acid and reported that the drying rate and therefore the drying constant values were found to be affected by the pretreatments. The objectives of this research were to determine the effect of temperature, and pre-treatment using hot water blanching and sodium meta-bisulphite on the drying kinetics of sweet potato slices in a convective air dryer.

2 Theorectical aspects

Drying is essentially a process of simultaneous heat and mass transfer (Dincer, 1998) and remains one of the most effective methods of preserving agricultural products. An understanding of the process is important because of the undesirable changes in the quality of dried products which may result if improperly implemented (Akpinar, Bicer and Midilli, 2003).

2.1 Mathematical model equations used for drying of agricultural products

A number of drying models have been reported in literature. Table 1 presents some of the mathematical models for thin layer drying of food materials.

No.	Model name	Model equation	Reference
1	Newton	$MR = \exp(-kt)$	Mujumdar and Menon (1995)
2	Logarithmic	$MR = a \exp(-kt) + c$	Yagcioglu, Degirmencioglu and Cagatay (1999)
3	Henderson and Pabis	$MR = a \exp(-kt) + c$	Zhang and Litchfield (1991)
4	Modified Henderson and Pabis	$MR = a\exp(-kt) + b\exp(-gt) + c\exp(-ht)$	Gunhan et al., (2005)
5	Approximation of Diffusion	$MR = a \exp(-kt) + (1-a) \exp(-kbt)$	Yaldiz and Ertekin (2001)
6	Page	$MR = \exp(-kt^n)$	Diamante and Munro (1993)
7	Modified Page 1	$MR = a \exp(-(kt)^n)$	Akpinar, Bicer and Midilli, (2003)
8	Two Term Exponential	$MR = a \exp(-kt) + (1-a) \exp(-kat)$	Sharaf-Eideen, Blaisdell and Hamdy (1980)
9	Wang and Singh	$MR = 1 + at + bt^2$	Wang and Singh (1978)
10	Midilli Kucuk &Yapar	$MR = a \exp(-kt^n) + bt$	Midilli, Kucuk and Yapar, (2002)

 Table 1
 Mathematical models for drying characteristics of products

Note: MR is dimensionless moisture ratio; a, b, k, t, n are coefficients.

Moisture ratio during drying experiment is usually calculated by using the following equation

$$MR = \frac{M_t - M_e}{M_o - M_e} \tag{1}$$

where, M_e is equilibrium moisture content, kg water/kg dry matter; M_o : initial moisture content (kg water/kg dry matter); M_t is moisture content at any time t, s.

The drying rate is calculated by using the following equation

$$D_R = \frac{M_{t+dt} - M_t}{D_t} \tag{2}$$

where, D_R is drying rate; M_t is as introduced earlier and M_{t+dt} is M_t after some incremental time d t; D_t is the elapsed drying time. Coefficient of determination (R^2) is the primary criterion for selecting the best equation to describe drying curve. Reduced chi square (χ^2) is the mean square of the deviation between the experimental and the predicted values for the models. The root mean square error (RMSE) is used to get the goodness of fit. The higher the values of R^2 , the lower the value of x^2 and the *RMSE*, hence the better of the goodness of fit (Yaldiz and Ertekin, 2001; Akpinar, Bicer and Midilli, 2003; Gunhan et al., 2005). They are calculated as

$$R^{2} = \frac{\sum_{i=1}^{n} (MR_{i} - MR_{pre,i}) \cdot \sum_{i=1}^{n} (MR_{i} - MR_{\exp,i})}{\sqrt{\left[\sum_{i=1}^{n} (MR_{i} - MR_{pre,i})^{2}\right] \left[\sum_{i=1}^{n} (MR_{i} - MR_{\exp,i})^{2}\right]}}$$
(3)

$$\chi^{2} = \frac{\sum_{i=1}^{n} \left(MR_{\exp,i} - MR_{pre,i} \right)^{2}}{N - z}$$
(4)

$$RMSE = \left[\frac{1}{z}\sum_{i=1}^{n} \left(MR_{pre,i} - MR_{\exp,i}\right)^{2}\right]^{\frac{1}{2}}$$
(5)

where, $MR_{exp,i}$ is the *ith* experimentally observed moisture ratio; $MR_{pre,i}$ is the *ith* predicted moisture ratio; N is the number of the observation; z is the number of constant in the model; n is a positive integer.

2.2 Effective moisture diffusivity and activation energy

The effective moisture diffusivity is calculated by using the simplified Fick's second law of diffusion model:

$$\frac{\partial M}{\partial t} = D_{eff} \nabla^2 M \tag{6}$$

where, *M* is moisture content (kg water/kg dry matter); *t* is the time s; D_{eff} is the effective moisture diffusivity, m²/s; ∇ is the differential operator. The solution of Fick's second law in slab geometry, with the assumption that moisture migration was caused by diffusion, negligible shrinkage, constant diffusion coefficient and temperature was given by Crank (1975) as follows:

$$MR = \frac{M_t - M_e}{M_o - M_e}$$

= $\frac{8}{\pi^2} \sum_{i=1}^{n} \frac{1}{(2n-1)^2} \exp\left(\frac{-(2n-1)^2 \pi^2 D_{eff} t}{4H^2}\right)$ (7)

where, *H* is the half thickness of the slab m; n = 1, 2, 3 ... the number of terms taken into consideration. For long drying time Equation (7) can be simplified further (Lopez et al., 2000; Doymaz, 2004) as:

$$MR = \frac{8}{\pi^2} \exp\left(\frac{-\pi^2 D_{eff} t}{4H^2}\right)$$
(8)

Activation energy is obtained by plotting the natural logarithm of D_{eff} against the reciprocal absolute temperature. Lopez et al., (2000) and Simal et al., (1996) related temperature with Arrhenius expression as

$$D_{eff} = D_o \exp\left(\frac{-E_a}{R(T+273.15)}\right)$$
(9)

where, D_o is the constant in Arrhenius equation, m²/s; E_a is the activation energy (kJ/mol); *T* is the temperature of air, °C; *R* is the universal gas constant, kJ/(mol · K).

Rearranging Equation (9) gives Equation (10):

$$\ln D_{eff} = \ln D_o - \frac{E_a}{R(T + 273.15)}$$
(10)

Energy of activation can thus be calculated from Equation (10), which gives a relationship between temperature and effective moisture diffusivity. The plot of ln*D* versus 1/(T+273.15) gives a straight line (slope of $K_L = E_a / R$). Linear regression analyses were used to fit the equation to the experimental data to obtain the coefficient of determination (R^2).

3 Materials and methods

3.1 Materials

Sweet potatoes tubers (centennial variety) were

purchased from a local market in Ikorodu, Lagos Nigeria. They were thoroughly washed in clean, potable water. A sharp stainless steel knife was used to peel the sweet potato under water to prevent browning. The sweet potatoes were cut into slices perpendicular to the main axis of the whole tuber. The thickness of the slices was (4 ± 0.02) mm but other dimensions in term of length and width were not kept constant for all the samples. Some samples were blanched in hot water at 100°C for 2 min and were labelled as "WAT". Some samples were sodium meta-bisulphite of 0.01% dipped into concentration at 100°C for 2 min (Tortoe et al., 2012) and were labelled as "SMB". Other samples were left untreated and were labelled as "UNT".

The drying behaviour was investigated in a convective hot air dryer (Model SAST 54, Jouan, France) at 50, 60, 70 and 80°C air drying temperatures with the air velocity fixed at 1.25 m/s. Low temperatures could result in prolonged drying while temperatures higher than the range specified could affect the physico-chemical properties and nutritional quality of any product made from sweet potato slices (Maruf, Akter and Jong-Bang, 2010). The drying system was run for at least 30 min to obtain steady conditions before placing the samples in the oven in thin single layer. Changes in weight of the slices were monitored at 30 min interval for the first 2 h and at 60 min interval thereafter. Further drying was stopped when changes in the weight of the samples with successive weighing time was no longer significant. The drying tests were conducted in duplicate at each air temperature for all the samples. Both blanched and unblanched sweet potato slices were analyzed for moisture content during drying. The initial weight before drying and the weight during the process at various times were recorded through the use of an analytical weighing balance (SARTORIOUS-CP 22025, Germany). Some samples for each treatment were kept from the start of drying and at the end for the purpose of moisture content estimation. The moisture content of the samples was determined using gravimetric oven method at 150°C for 5 h (AOAC, 1990).

3.2 Mathematical modelling and drying curves

The MR of the sweet potato slices during thin layer

drying experiment was calculated by using Equation (3). Four of the popular thin layer drying models reported to have performed well for roots and tubers (Tunde-Akintunde and Afon, 2009; Mayor and Sereno, 2004), namely Modified Page 1, Approximation of Diffusion, Two Term Exponential and Wang and Singh were selected and fitted to the data. Regression analysis was performed using Data Fit (Oakdale Engineering, 2008). The primary criterion for selecting the best equation to describe the drying curve was coefficient of determination (R^2).

3.3 Determination of effective moisture diffusivity and activation energy

The effective moisture diffusivity of the samples was estimated by using the simplified mathematical Fick's second diffusion model (Equation 8). The activation energy of the samples was obtained by plotting the natural logarithm of D_{eff} against the reciprocal of absolute temperature, then determining the slope of the straight line by using Equation (10).

4 **Results and discussion**

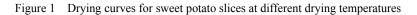
The time to reach about 10% dry basis (d.b.) moisture content from the initial moisture content of about 294% (d.b.) was found to be between 300 min and 360 min. A relatively high drying rate was observed within the first 90 min of the drying time, but as drying progressed, the moisture ratio was observed to decrease non-linearly with the increase in drying time for all samples (as shown in Figure 1). The drying of sweet potato slices exhibited the characteristic moisture desorption behaviour noted for many tuber crops (Tunde-Akintunde and Afon, 2009), which has been explained to be due to various forms in which water is present in food products.

4.1 Effect of temperature and pre-treatments

It was observed that increase in drying temperature reduced the drying time and vice versa. As shown in Figure 2, the drying rate values (g water/100 g DM hr) are significantly higher at the higher temperature (80° C) than at the lower (50° C). Besides, no constant drying period was observed. These results are in agreement with earlier observations for various fruits, roots and vegetables (Kajuna et al, 2010, Tunde –Akintunde and

SMB WAT - UNT 1.2 1.2 1.0 1.0 0.8 0.8 Moisture ratio Moisture ratio 0.6 0.6 0.4 0.4 0.2 0.2 0 0 0 30 60 90 120 150 180 0 30 60 90 120 150 Time/min Time/min a. 50 °C b. 60 °C 1.2 1.2 1.0 1.0 0.8 0.8 Moisture ratio Moisture ratio 0.6 0.6 0.4 0.4 0.2 0.2 0 0 0 30 60 90 120 150 180 0 30 60 90 Time/min Time/min c. 70 ℃ d. 80 °C

Afon, 2009; Sacilik, Keskin and Elicin, 2006, and Doymaz, 2005).



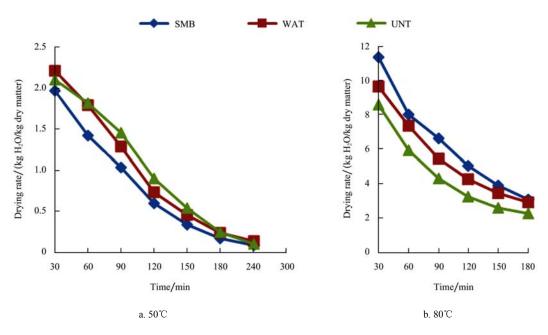


Figure 2 Drying rate curves for different pre-treatments

Figure 2 indicates that pre-treatments also affect the drying rate of sweet potato slices. At the lower temperature (50° C), the drying rate was only marginally different for the different pre-treatment schemes. At the higher temperature (80° C) however, the effects of the pre-treatment effects became more obvious, resulting in higher drying rates for both SMB and WAT. This shows that although pre-treatment reduces the resistance to moisture transport thereby increasing the drying rates, the effects are felt more at higher temperatures than at lower.

4.3 Mathematical modelling of drying of sweet potato slices

The result of the regression analysis performed to fit the experimental data to the selected thin layer drying models (Modified Page 1, Approximation of Diffusion, Two Term Exponential and Wang and Singh) are shown in Table 2. Based on the model with the highest R^2 , the lowest χ^2 and lowest *RMSE*, the Page's model gave a better correlation between the moisture ratio and drying time of sweet potato slices under the conditions of the experiments.

Table 2 Regression analysis and fitting of experimental data to drying model	Table 2	Regression	analysis and	fitting of ex	xperimental (data to drying models	5
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Model name	Treatment	Parameters	R^2	χ ²	RMSE
	SMB at 50°C	a = 0.989, k = 5.832, n = 0.573	0.99907	0.000183	0.0060618
	SMB at 60°C	a = 0.999, k = 7.784, n = 1.266	0.99992	0.000062	0.0039545
	SMB at 70°C	<i>a</i> =0.999, <i>k</i> =9.901, <i>n</i> =1.175	0.99985	0.000119	0.0054586
	SMB at 80°C	<i>a</i> =0.995, <i>k</i> =9.934, <i>n</i> =1.142	0.99988	0.000367	0.0763802
	WAT at 50°C	<i>a</i> =0.991, <i>k</i> =4.656, <i>n</i> =1.064	0.99495	0.048582	0.3532192
Mediced Decent	WAT at 60°C	<i>a</i> =0.998, <i>k</i> =7.567, <i>n</i> =1.252	0.99969	0.000242	.00779381
Modified Page 1	WAT at 70°C	a = 1.000, k = 1.259, n = 1.157	0.99970	0.000246	0.0078440
	WAT at 80°C	<i>a</i> =0.999, <i>k</i> =9.231, <i>n</i> =1.378	0.99847	0.002703	0.0130266
	UNT at 50℃	<i>a</i> =0.991, <i>k</i> =4.655, <i>n</i> =1.246	0.99907	0.002298	0.0295290
	UNT at 60℃	<i>a</i> =0.995, <i>k</i> =7.100, <i>n</i> =1.357	0.99879	0.000998	0.0157978
	UNT at 70℃	<i>a</i> =0.998, <i>k</i> =9.994, <i>n</i> =1.285	0.99978	0.000182	0.0067560
	UNT at 80℃	<i>a</i> =0.999, <i>k</i> =1.044, <i>n</i> =1.196	0.99964	0.000114	0.0030669
	SMB at 50℃	<i>a</i> =-7.497, <i>b</i> =0.971, <i>k</i> =1.707	0.99071	0.008785	0.03542602
	SMB at 60°C	a = -6.20, b = 0.899, k = 1.516	0.99986	0.000109	0.0052305
	SMB at 70°C	a = -6.984, b = 0.928, k = 1.70	0.99984	0.000129	0.0056923
	SMB at 80°C	a = -6.141, b = 0.804, k = 1.80	0.99796	0.001072	0.0165399
	WAT at 50°C	<i>a</i> =-4.445, <i>b</i> =0.936, <i>k</i> =6.62	0.99578	0.003777	0.0232922
Approximation of	WAT at 60°C	a = -8.234, b = 0.925, k = 1.42	0.99965	0.000282	0.0084010
Diffusion	WAT at 70°C	a = -6.908, b = 0.229, k = 0.22	0.99989	0.000088	0.0047094
	WAT at 80°C	<i>a</i> =-3.767, <i>b</i> =0.705, <i>k</i> =7.49	0.98970	0.004884	0.0506012
	UNT at 50°C	<i>a</i> =-4.864, <i>b</i> =0.885, <i>k</i> =8.87	0.99869	0.001315	0.0013710
	UNT at 60℃	a=6.149, b=0.885, k=0.014	0.99822	0.001465	0.0191376
	UNT at 70°C	<i>a</i> =-9.838, <i>b</i> =0.931, <i>k</i> =1.941	0.99966	0.000285	0.0084432
	UNT at 80°C	<i>a</i> =-6.132, <i>b</i> =0.461, <i>k</i> =1.309	0.99871	0.007548	0.0191065
	SMB at 50°C	<i>a</i> =3.305, <i>k</i> =1.258	0.98147	0.017524	0.0468033
	SMB at 60℃	<i>a</i> =2.575, <i>k</i> =3.137	0.98918	0.008737	0.0418023
	SMB at 70°C	a=4.721, k=2.025	0.99687	0.002513	0.0224231
	SMB at 80°C	<i>a</i> =4.062, <i>k</i> =1.162	0.99672	0.005980	0.0460179
	WAT at 50°C	a = 2.691, k = 2.914	0.99455	0.004878	0.0246948
Two Term Exponential	WAT at 60°C	a = 4.987, k = 2.603	0.98977	0.008143	0.0403579
	WAT at 70°C	<i>a</i> =4.129, <i>k</i> =2.021	0.99757	0.001974	0.0198708
	WAT at 80°C	a=2.055, k=2.347	0.98790	0.006539	0.0562635
	UNT at 50℃	<i>a</i> =2.127, <i>k</i> =3.500	0.98746	0.012626	0.0397277
	UNT at 60℃	<i>a</i> =2.941, <i>k</i> =3.576	0.98065	0.015951	0.0564820
	UNT at 70℃	<i>a</i> =4.527, <i>k</i> =2.335	0.99099	0.007628	0.0390593
	UNT at 80℃	a = 2.655, k = 2.347	0.99987	0.000934	0.0070977

Model name	Treatment	Parameters	R^2	χ^2	RMSE
	SMB at 50°C	<i>a</i> =-3.147, <i>b</i> =2.572	0.99552	0.004238	0.0230176
	SMB at 60°C	<i>a</i> =-5.921, <i>b</i> =8.994	0.99870	0.001050	0.0144959
	SMB at 70°C	<i>a</i> =-6.938, <i>b</i> =1.187	0.98741	0.010096	0.0449376
	SMB at 80°C	<i>a</i> =-7.386, <i>b</i> =1.330	0.99977	0.000926	0.0018755
	WAT at 50°C	<i>a</i> =-0.004, <i>b</i> =3.451	0.98916	0.009699	0.0348203
Wang and Sinch	WAT at 60°C	<i>a</i> =-5.777, <i>b</i> =8.599	0.99884	0.000916	0.0013542
Wang and Singh	WAT at 70°C	<i>a</i> =-7.894, <i>b</i> =1.479	0.96600	0.027651	0.0743653
	WAT at 80°C	<i>a</i> =-6.925, <i>b</i> =1.148	0.99859	0.006017	0.0875537
	UNT at 50°C	<i>a</i> =-3.599, <i>b</i> =3.363	0.99917	0.000835	0.0102215
	UNT at 60°C	<i>a</i> =-5.428, <i>b</i> =7.462	0.99955	0.000373	0.0086473
	UNT at 70℃	<i>a</i> =-7.079, <i>b</i> =1.221	0.99322	0.005744	0.0338963
	UNT at 80°C	<i>a</i> =-8.337, <i>b</i> =1.893	0.99887	0.007611	0.0831376

4.4 Effective moisture diffusivity

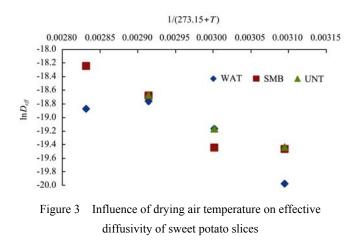
The effective moisture diffusivity of the samples obtained is shown in the Table 3. The effective moisture diffusivity (Deff) for drying SMB, WAT and UNT samples ranged between 1.20×10^{-8} and $7.76 \times$ 10^{-9} m²/s. Similar result have been obtained for other agricultural crops like organic tomatoes: 2.56×10-9-4.28×10⁻⁹ and 4.29×10⁻⁹-6.28×10⁻⁹ m²/s (Sacilik, Keskin and Elicin, 2006); yam slices: $7.62 \times 10^{-8} - 9.06 \times 10^{-8} \text{ m}^2/\text{s}$ (Sobukola, Dairo and Odunewu, 2008); okra: 1.125× $10^{-9}-9.93 \times 10^{-9}$ m²/s and $1.165 \times 10^{-8}-7.13 \times 10^{-9}$ m²/s for treated and untreated samples respectively (Sobukola, 2009). Thus the diffusivity values obtained from the experimental data fall within the $(10^{-11}-10^{-6} \text{ m}^2/\text{s})$ range reported for most food products (Doymaz, 2007; Tunde-Akintunde, 2009).

Table 3 Effective moisture diffusivity for differentpre-treatment methods at various drying temperatures

Pretreatment	Air temperature/°C	$D_{eff}/\mathrm{m}^2\cdot\mathrm{s}^{-1}$	
SMB	50	3.63×10 ⁻⁹	
WAT	50	2.11×10 ⁻⁹	
UNT	50	7.08×10 ⁻⁸	
SMB	60	4.76×10 ⁻⁹	
WAT	60	4.76×10 ⁻⁹	
UNT	60	3.59×10 ⁻⁹	
SMB	70	7.76×10 ⁻⁹	
WAT	70	7.12×10 ⁻⁹	
UNT	70	7.73×10 ⁻⁹	
SMB	80	1.09×10 ⁻⁹	
WAT	80	6.40×10 ⁻⁹	
UNT	80	1.20×10^{-8}	

Moisture diffusivity, which is related to the quantity of heat passing normally through a unit area per unit time, is also affected by drying temperatures, as increasing the air temperature resulted in higher effective moisture diffusivity as shown in Table 3. Thus, energy consumption is expected to decrease as temperature increases at constant air velocity. This result is similar to the findings of Kouchakzadeh (2010) for pistachios and Motevali et al., (2012) for jujube. **4.5** Activation energy

The influence of temperature on the effective diffusivity was obtained by plotting $\ln D_{eff}$ against () is as shown in Figure 3 for SMB, WAT and UNT samples. From the slope of the graph, the activation energy was observed to be 11.25 kJ/mol, 9.13 kJ/mol and 17.5 kJ/mol for treated SMB, WAT and UNT samples, respectively.



The result of the activation energy was found to be 11.25 kJ/mol, 9.13 kJ/mol and 17.5 kJ/mol for treated SMB, WAT and UNT samples respectively. From the result, it was clearly observed that there was lower activation energy for the pre-treated samples (SMB and WAT) than for the untreated samples UNT. This indicates that it was easier to induce the water release process in the WAT and the SMB compared to the UNT samples. Similar results have been reported by Doymaz (2007).

5 Conclusions

This study evaluates the effects of pre-treatment on the drying characteristics of sweet potato slices. The experimental drying data were fitted to four well known drying models, includes the Modified Page 1, Wang and Singh, Two Term Exponential and Approximation of Diffusion. The following conclusions are drawn from the present study:

1) The drying of sweet potato slices exhibited higher drying rates for pre-treated samples than for untreated samples, especially at higher temperatures.

2) The R^2 values for Modified Page's model were

higher and the χ^2 and RMSE values were lower than that from the other three models. Modified Page's model is therefore judged to have performed best in describing the drying curve of sweet potato slices under the considered experimental conditions.

3) The effective moisture diffusivity for SMB, WAT and UNT samples ranged between 0.12×10^{-9} and 7.76×10^{-9} m²/s, increasing the air temperature resulted in the higher effective moisture diffusivity.

4) There was lower activation energy for the pretreated samples (SMB and WAT) than for the untreated samples UNT. The result of the activation energy was found to be 11.25 kJ/mol, 9.13 kJ/mol and 17.5 kJ/mol for treated SMB, WAT and UNT samples respectively. This indicates that it was easier to induce the water release process in the WAT and the SMB compared to the UNT samples.

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